



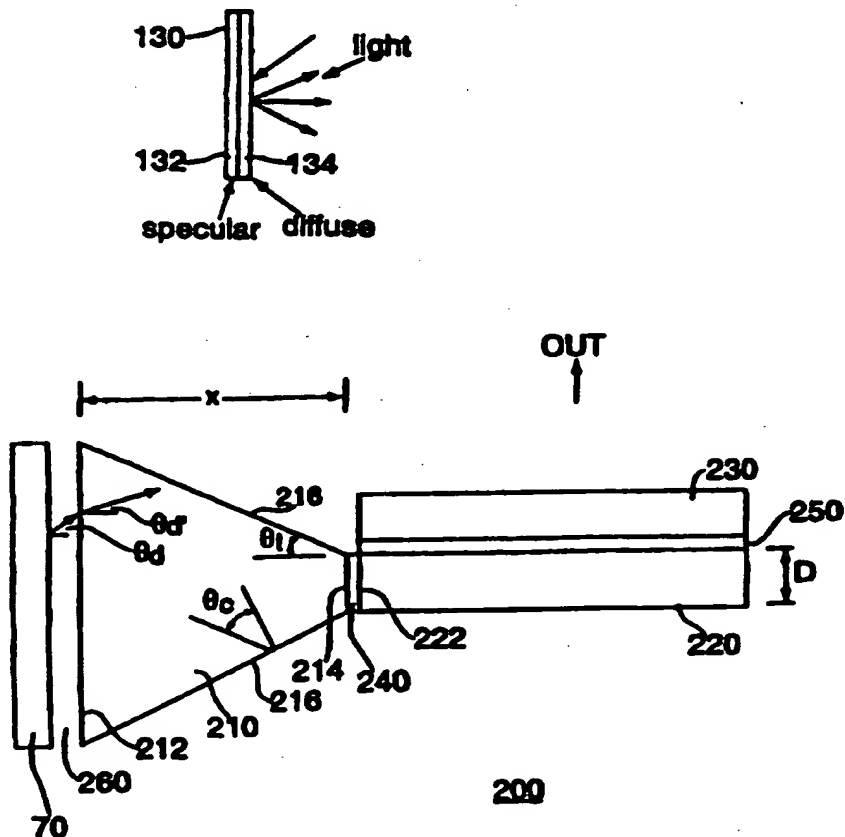
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(71) Applicant: ALLIEDSIGNAL INC. [US/US]; 101 Columbia Road, P.O. Box 2245, Morristown, NJ 07962-2245 (US).			
(72) Inventors: UNGER, Waltraud, Rosalie; 9 Warren Place, Glen Rock, NJ 07452 (US). ZIMMERMAN, Scott, Moore; 41 Carlisle Road, Basking Ridge, NJ 07920 (US). KUPER, Jerry, W.; 1336 Tullo Road, Martinsville, NJ 08836 (US). CHIN, Tim; 3233 Delta Road, San Jose, CA 95135 (US).			
(74) Agent: CRISS, Roger, H.; AlliedSignal Inc., Law Dept. (C.A. McNally), 101 Columbia Road, P.O. Box 2245, Morristown, NJ 07962-2245 (US).			

**(54) Title: ILLUMINATION SOURCES AND SYSTEMS**

**(57) Abstract**

The reflectivity of a substrate (40) can be improved by combining a reflective diffuse layer (139) with a specular layer (132). The light output of individual light sources (70) can be improved by embedding them in a composite diffuse and specular substrate (40) resulting in a superior illumination source. A tapered coupling waveguide (210) having a large input surface (212) can be used to couple the illumination source (70) to a thin waveguide (220) having a relatively small input surface area (222).



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## ILLUMINATION SOURCES AND SYSTEMS

### Background of the Invention

For certain applications, a back-lit illumination system having a very shallow depth is highly desirable. Such systems are commonly configured with one or more light sources, a waveguide for collecting and distributing the light from the light source, and a collimating apparatus for extracting the light from the waveguide. A significant depth savings can be achieved by coupling the light source through the edge of the waveguide.

The amount of light extracted from the system is proportional to the number of reflections or bounces that occur within the waveguide, the number being inversely proportional to the thickness of the waveguide. To obtain maximum light output, a thin waveguide is preferable. However, this results in edges having a small surface area, limiting the size of the light source that can directly adjoin the edge of the waveguide. On the other hand, if the surface area of the edge is increased, the extraction efficiency of the waveguide will decrease.

It would be highly desirable to utilize a thin waveguide yet provide maximum light source input. Further, a highly reflective and powerful light source would also be desirable.

### Brief Description of Drawings

The invention will be more fully understood and further advantages will become apparent when reference is made to the following detailed description of the invention and the accompanying drawings in which:

5        Figure 1 is a schematic drawing of an illumination source having an array of light sources embedded in reflective material;

      Figure 2 is a schematic cross-sectional diagram of an illumination system utilizing the illumination source of Figure 1 and a waveguide;

      Figure 3 is a schematic drawing of the illumination source of Figure 1  
10        having a two-dimensional array of light sources embedded in reflective material;

      Figures 4-7 illustrate the reflective behavior of diffuse and specular materials of varying thicknesses and in combination;

      Figures 8 and 9 are cross-sectional and plan view diagrams, respectively, of an illumination system utilizing the illumination source of Figure 3; and

15        Figure 10 is a plan view diagram of an alternative illumination system utilizing the illumination source of Figure 3.

### Description of the Invention

20        A thin waveguide can be used without sacrificing light input by coupling a large light source, or multiple light sources, to the waveguide edge through a coupling structure (e.g., a second waveguide) that tapers down from the light

source to the dimensions of the waveguide edge. The broad face of the input to the coupling structure permits one to couple multiple sources (or a large light source) into the waveguide.

5 The performance of illumination systems can be further enhanced by using highly reflective substrates that combine the reflective qualities of both diffuse and specular materials. When used in combination, the thickness of the composite substrate can be significantly reduced and the reflectivity increased. Additionally, a superior illumination source offering high efficiency can be achieved by embedding planar light sources in the substrate.

10 As illustrated in Figure 1, an illumination source 10 that can be used with the illumination system described here contains an array 20 of one or more light sources 30 such as light emitting diodes (LEDs), flat fluorescent lamps, electroluminescent sources, or some other planar source suitable to the application embedded in a substrate 40 of highly reflective diffuse material. The  
15 illumination source 10 may be coupled to a waveguide as shown by the end views of the two illumination sources 10 adjacent the waveguide 50 in Figure 2. The arrows 60 represent the dispersion of light rays received from the illumination source 10 within the waveguide 50.

20 Typically, the light sources 30 constitute a fraction of the total surface area of the substrate 40, ranging from about 10% to about 70%, and preferably from about 10% to about 30%. In addition to the linear arrangement of Figures

1 and 2, the light sources 30 could be configured in other layouts such as the two-dimensional array 70 of Figure 3. Other shapes and configurations may be utilized (e.g., triangular, circular, hexagonal, etc.), as will readily occur to those skilled in the art. Although 5 mm spacing has been successfully  
5 employed, the spacing can range from about 0.25 millimeters to about 3 centimeters, depending on the brightness of the light source employed.

The light sources can be mounted on any suitable surface such as a copper-coated, glass-fiber board and spaced apart to achieve the desired luminance. Depending on thermal management needs, other mounting  
10 structures such as diamond or sapphire film can be used, as will readily occur to those skilled in the art.

The light sources 30 are affixed to an underlying board by soldering or some other suitable means as will readily occur to those skilled in the art. The substrate 40 is then provided with openings that conform to the outline of the  
15 light sources 30, allowing the light emitted by the light sources 30 to pass through the substrate 40. Alternatively, the light sources 30 could be placed on top of the substrate 40 and the electrical connections brought through.

Surface-mount LEDs having a size of approximately one millimeter square may be employed as the light sources, although other types and sizes of  
20 LEDs could be selected, as will be readily apparent to those skilled in the art. Suitable LEDs are commercially available from Dialight Corporation of

Manasquan, N.J., Hewlett-Packard, and Nichia Chemical. Depending on the application, light sources of a single color (e.g., red, green, yellow, blue) or of multiple colors may be employed.

To obtain the desired degree of reflectance, the substrate 40 must have sufficient depth. Materials exhibiting a very high reflectance, i.e., approaching 100%, for visible light, consist of diffuse scattering media with little or no absorption in the visible range. One example of a substrate having sufficient depth is the thick layer 100 of reflective diffuse material shown in the schematic cross-sectional diagram of Figure 4. Where the thickness of the layer 100 of diffuse material is about 0.51 mm or greater, at least about 95% of the light is reflected at the surface 102.

If the material is not sufficiently thick, a portion of the light energy will pass through the layer rather than be reflected. For example, for thicknesses of less than 0.2 mm, the reflectance for diffuse materials is low, typically less than 90%. As compared to the layer of Figure 4, the relatively thin layer 110 of reflective diffuse material of Figure 5 thus reflects a smaller percentage of the incident light rays. Although the specular material of the thin reflective layer 120 of Figure 6 will reflect approximately 80-95% of the incident light rays, it behaves like a mirror, and therefore diffuse material is preferred as it scatters the incident light rays.

Since space is limited in many applications, it is desirable to combine the scattering effects of diffuse material with the shallow depth of specular material.

One such combination is the composite reflector 130 shown in Figure 7, having a thin specular backing layer 132 behind a thin diffuse scattering layer 134. The two layers 132 and 134 may be joined by simply placing them together, relying on surface tension, bonding, adhesion, or lamination, the latter being the preferred method of joining the two layers. Alternatively, the specular layer 132 can be sputtered onto the diffuse layer 134 or provided as a coating on the diffuse layer 134.

The benefit of providing a specular layer 132 behind a diffuse layer 134 is realized whenever the thickness of the diffuse layer 134 is less about 0.5 mm.

In such instances, depending on the specific materials employed, the addition of the specular layer 132 layer can increase the reflectance to at least about 97%.

A composite reflector 130 having an 0.2 mm thick diffuse layer of PTFE material and a 0.076 mm thick specular layer of silver film provided comparable results. The thickness of the specular layer 132 layer may range from about 0.25  $\mu\text{m}$  to about 0.1 mm, depending on the materials used and the method of manufacture (e.g., sputtering).

It should be understood that other thicknesses and relative ratios could be employed as will be readily apparent to those skilled in the art. The composite reflector 130 of Figure 7 may be employed in place of the substrate 40 in the



illumination source 10 of Figures 1 and 2, resulting in a decrease of the physical depth required for the substrate when compared to substrates that are purely diffuse.

Diffuse materials suitable for the applications discussed here are Spectralon from Labsphere, Inc. and PTFE (Teflon) film from Furon or E.I. du Pont de Nemours & Co. Specular materials include Silverlux™, a product of 3M, and other highly-reflective (i.e., greater than 90% reflectance) materials such as aluminum, gold, and silver, as well as others as will readily occur to those skilled in the art. The reflectivity of any of the materials discussed may be measured using several commercially available instruments such as the Macbeth #7100 Spectrophotometer, New Windsor, N.Y., or a Perkin Elmer #330 Spectrophotometer, Danbury, CT. The specular materials may be deposited on a secondary surface or directly on the diffuse material by such techniques as chemical vapor deposition, electron beam vapor deposition, sputtering, and the like.

The output of the illumination source 70 of Figure 3 may be used in an illumination system by coupling the light through a tapered coupling waveguide. In the illumination system 200 shown in the schematic cross-sectional view of Figure 8, an illumination source 70 having a two-dimensional array of light sources is positioned adjacent the input surface 212 of a tapered coupling waveguide 210. Light leaves the tapered coupling waveguide 210 through an

output surface 214, where it enters an output waveguide 220 through an edge input surface 222. In turn, the output waveguide 220 provides light energy to a light collimating assembly 230. The drawing in Figure 8 is not drawn to scale; the actual relative dimensions may vary depending on the application.

5           An optically-transparent adhesion layer 240 located between the tapered coupling waveguide 210 and the edge input surface 222 of the output waveguide 220 insures maximum light transfer. The layer 240 can be made from any optically clear material having an index of refraction preferably substantially equal to that of the waveguides 210 and 220. Alternatively, the two waveguides  
10       210 and 220 may be thermally fused or fused by a solvent using materials and techniques well known in the art. As desired and appropriate, adhesion layers may be employed between other components of the illumination system 200, e.g., between the output waveguide 220 and the light collimating assembly 230.

15       A similar adhesion layer 250 is provided between the output waveguide 220 and the light collimating assembly 230. Again, the output waveguide 220 and the light collimating assembly 230 may be thermally fused or fused by a solvent.

20       At the junction of the illumination source 70 and the tapered coupling waveguide 210, an air gap 260 is provided to maximize refraction of the light as it enters the tapered coupling waveguide 210. Preferably, the air gap 260 is at least several wavelength in thickness, to permit refraction of the light travelling from the illumination source 70 into the tapered coupling waveguide 210.

The waveguides 210 and 220 and associated structure, including the adhesion layers, may be fabricated according to the methods and using such materials as polycarbonate, acrylic, polystyrene, glass, transparent ceramics, and a monomer mixture disclosed in U.S. Patent No. 5,396,350, issued March 7, 1995, to Beeson et al., for a Backlighting Apparatus Employing an Array of Microprisms, U.S. Patent No. 5,448,468, issued June 27, 1995, to Zimmerman et al., for an Illumination System Employing an Array of Microprisms, U.S. Patent No. 5,462,700, October 31, 1995, to Beeson et al., for a Process for Making an Array of Tapered Photopolymerized Waveguides, and U.S. Patent No. 5,481,385, issued January 2, 1996, to Zimmerman et al., for a Direct View Display with Array of Tapered Waveguide, all of which are incorporated herein by reference.

The thickness D of the output waveguide 220 is kept small to maximize the number of reflections or bounces of light that enters from the output surface 214. The thickness D may range from about 0.5 to about 10 mm; typically, thicknesses from about 6 to about 8 mm have been employed. If light enters only through one edge, one may wish to provide a slight taper in the output waveguide 220 on the surface away from the collimating assembly 230 to optimize the number of bounces and therefore enhance the throughput of the output waveguide. The angle of taper may range from about  $0.25^\circ$  to about  $2.0^\circ$ ; the actual angle is dependent on the length of the waveguide 220.

Optimally, total internal reflection (TIR) channels all of the light entering the tapered coupling waveguide 210 to the output surface 214. To accept the greatest amount of light, the input surface 212 of the tapered coupling waveguide 210 is made as large as possible. However, as the area of the input surface 212 increases with respect to the output surface 214, increasing the taper angle  $\Theta_t$ , increasing amounts of light are likely to pass through one of the tapered surfaces 216 of the tapered coupling waveguide 210, especially if the individual LEDs have a wide output angular distribution. This occurs because the incident light rays strike those surfaces at less than the critical angle, defined as  $\Theta_c$ , where  $\Theta_c = \sin^{-1}(n_1/n_2)$ , normal to the tapered surface 216, and where  $n_2$  is the index of refraction of the tapered coupling waveguide 210 and  $n_1$  is the index of refraction of the material (e.g., air) outside of the tapered coupling waveguide 210. To avoid loss of light through failure of TIR, the taper angle  $\Theta_t$  must be minimized as much as possible while still providing an input surface 212 of sufficient area.

To select a taper angle  $\Theta_t$ , the designer must consider the angular distribution ( $\pm \Theta_d$ ) of the output of the light sources, the indices of refraction of the tapered coupling waveguide 210 and the surrounding medium, and the maximum acceptable light loss. The taper angle  $\Theta_t$  can be derived from Snell's Law and the equation for the critical angle.

Assume that the LEDs have an output of  $\pm \Theta_d$ . When the light rays from the LEDs enters the tapered coupling waveguide 210, the propagation angle is modified ( $\pm \Theta_d$ ) according to the relative index of refraction, as set forth in Snell's Law:

$$5 \quad n_1 \sin \Theta_d = n_2 \sin \Theta_d'.$$

Solving for  $\Theta_d'$ ,

$$\Theta_d' = \sin^{-1} (n_1/n_2 \sin \Theta_d).$$

Light rays at the extreme angle  $\Theta_d'$  impact a tapered surface 216 at an incident angle of  $90^\circ - (\Theta_i + \Theta_d')$  from the normal (with respect to the tapered surface 216). After reflection, the rays then impact the opposite tapered surface 216 at an incident angle of  $90^\circ - (2\Theta_i + \Theta_d')$  from the normal (with respect to the other tapered surface 216). In both cases, the incident angle must be greater than the critical angle to reflect.

Based on the foregoing, one can set forth the following generalized equation for determining the incident angle:

$$15 \quad \Theta_i = 90^\circ - [(2(r-1) + 1) \cdot \Theta_i + \Theta_d']$$

where  $r$  is the number of reflections of the light rays.

Given the equation for  $\Theta_i$ , to insure that the light remains in the tapered coupling waveguide,  $\Theta_i$  must be selected such that

$$\theta_i > \theta_c$$

or

$$90^\circ - [(2(r-1) + 1) \cdot \theta_i + \theta_d] > \sin^{-1} (n_1/n_2)$$

Solving for  $\theta_i$ ,

$$\theta_i < [90^\circ - \theta_d - \sin^{-1} (n_1/n_2)]/[2(r-1) + 1].$$

With this last relationship, a taper angle can be selected based on the LEDs employed, the relative index of refraction, and the number of reflections that will occur.

As a tradeoff, the size of the input surface can be enlarged to the point where a certain portion of the outer extremities of the LED radiation pattern is forfeited. Thus, while a certain percentage of the light output of the LEDs passes directly out of the tapered coupling waveguide 210, TIR keeps the majority of the light rays in the tapered coupling waveguide 210 and channels it to the output waveguide 220. The relationships discussed above can be used to optimize the light input achieved by increasing the size of the input surface 212 of the tapered coupling waveguide 210 against critical angle loss.

The illumination system 200 is shown again in the plan view diagram of Figure 9. By adding from one to as many as three additional illumination sources 70 and associated tapered coupling waveguides 210, even more light energy can be provided to the output waveguide 220, as illustrated in Figure 10. It should be understood from Figures 8, 9, and 10 that the tapered coupling

waveguides 210 can be tapered in more than one direction, e.g., in both the x and y directions.

The distribution angle of the LEDs can be minimized by placing converging lenses over each LED. Such lenses are typically provided by the manufacturer of the LEDs; in some instances, the lenses are an integral part of the LED package.

In an alternative embodiment of the illumination system of Figures 8, 9, and 10, the tapered coupling waveguide 210 could be a hollow structure having mirrored specular surfaces for achieving reflection within the waveguide 210. The surfaces can be fabricated through a coating process or a sputtering process, or some other method as will readily occur to one skilled in the art. In another alternative embodiment, a commercially-available tapered fiber-optic bundle could be substituted for the solid or hollow tapered coupling waveguide 210.

It should be understood that this invention is applicable to a wide variety of devices such as direct illumination devices including lighting for commercial, office, residential, outdoor, automotive, and appliance applications. The invention may also be applied to displays for computer, automotive, military, aerospace, consumer, commercial, and industrial applications, and any other device requiring improved reflective materials to obtain an efficient illumination source.

While there has been described what is believed to be the preferred embodiment of the invention, those skilled in the art will recognize that other and further modifications may be made thereto without departing from the spirit of the invention, and it is intended to claim all such embodiments that fall within  
5 the true scope of the invention.



1       A reflector, comprising:

(a) a first layer of diffuse, reflective material; and

(b) a second layer of specular, reflective material adjacent the first layer

5       2.       An illumination source, comprising:

(a) a substrate of reflective material; and

(b) at least one planar light source affixed to the substrate.

3.       An illumination system, comprising:

10       (a) an illumination source comprising (i) a substrate of reflective material,

and (ii) at least one planar light source affixed to the substrate; and

(b) a waveguide having an output surface and at least one edge input surface generally perpendicular to the output surface, where the edge input surface is adjacent the illumination source.

15

4.       An illumination system as set forth in claim 3, wherein the light

source is a light emitting diode, flat fluorescent lamp, or an electroluminescent source.

20

5.       An illumination system as set forth in claim 3, wherein there are a

plurality of light sources arranged in a two-dimensional array.

6. An illumination system, comprising:

(a) an illumination source comprising

(i) a substrate of reflective material; and

5 (ii) at least one planar light source affixed to the substrate, the substrate having a surface area;

(b) a generally planar output waveguide, the output waveguide having an output surface and at least one edge input surface generally perpendicular to the output surface, where the edge input surface has a surface area substantially less  
10 than the surface area of the substrate of the illumination source; and

(c) a tapered coupling waveguide for coupling the output of the illumination source to the edge input surface of the output waveguide, the coupling waveguide comprising

(i) an input surface for accepting the output of the illumination  
15 source, the input surface having a surface area approximately equal to and symmetrical with respect to at least a portion of the surface area of the substrate of the illumination source; and

(ii) an output surface for providing light to the edge input surface of the output waveguide, the output surface having a surface area approximately  
20 equal to and symmetrical with respect to at least a portion of the surface area of the edge input surface of the output waveguide.

7. An illumination system as set forth in claim 6, wherein there are a plurality of light sources arranged in a two-dimensional array.

5 8. An illumination system as set forth in claim 6, wherein the substrate comprises a layer of diffuse, reflective material.

9. An illumination system, comprising:

(a) an illumination source comprising

10 (i) a substrate having a surface area, the substrate being fabricated from reflective material comprising a layer of diffuse, reflective material and an additional layer of specular, reflective material adjacent the layer of diffuse, reflective material; and

(ii) a plurality of light emitting diodes embedded in the substrate and  
15 arranged in a two-dimensional array;

(b) a generally planar output waveguide, the output waveguide having an output surface and at least one edge input surface generally perpendicular to the output surface, where the edge input surface has a surface area substantially less than the surface area of the substrate of the illumination source; and

(c) a tapered coupling waveguide for coupling the light of the illumination source to the edge input surface of the output waveguide, the coupling waveguide comprising

5 (i) an input surface for accepting the output of the illumination source, the input surface having a surface area approximately equidimensional and symmetrical with respect to the surface area of the substrate of the illumination source; and

10 (ii) an output surface for providing light to the edge input surface of the output waveguide, the output surface having a surface area approximately equidimensional and symmetrical with respect to the surface area of the edge input surface of the output waveguide.

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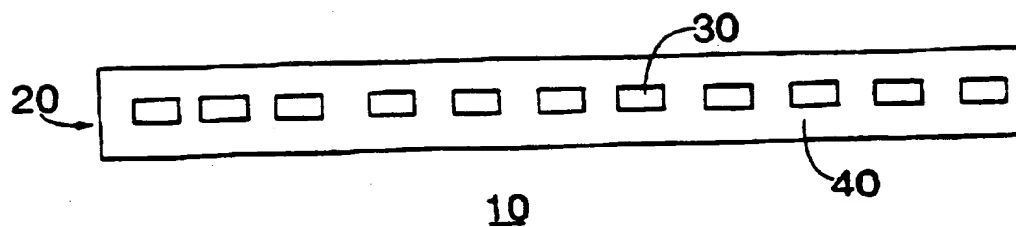


FIG. 1

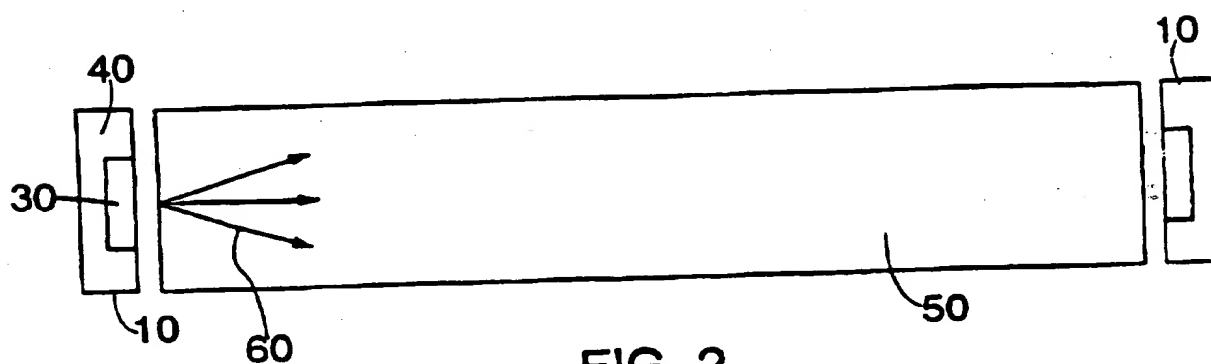


FIG. 2

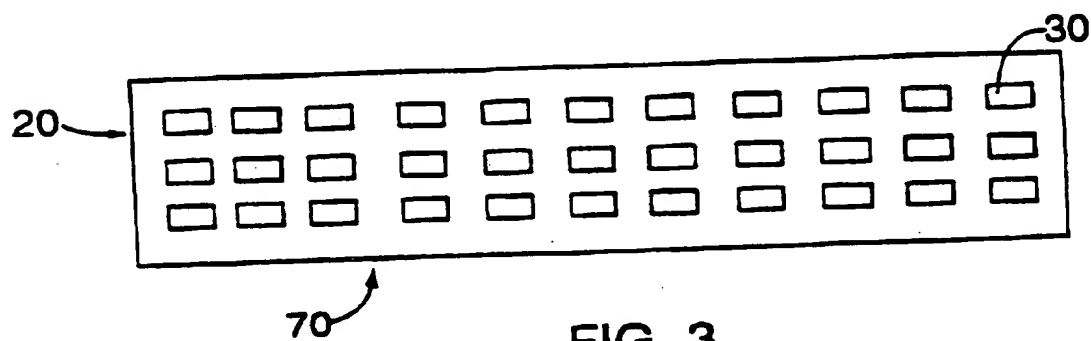


FIG. 3

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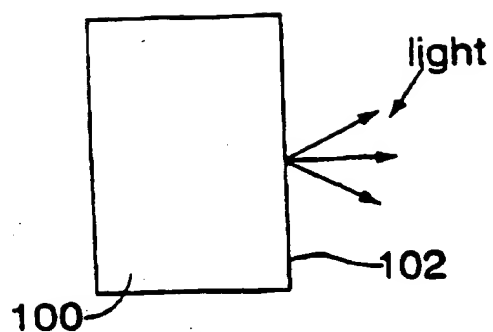


FIG. 4

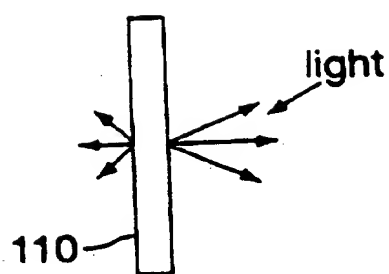


FIG. 5

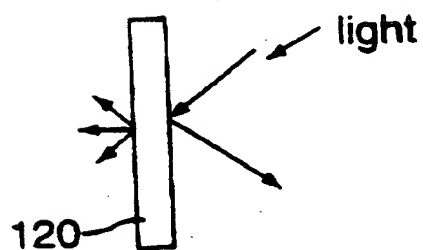


FIG. 6

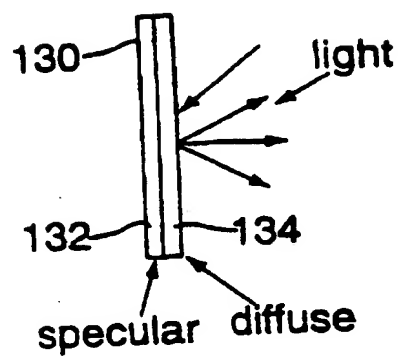


FIG. 7

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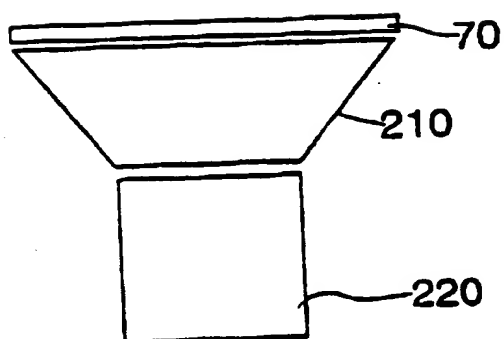


FIG. 9

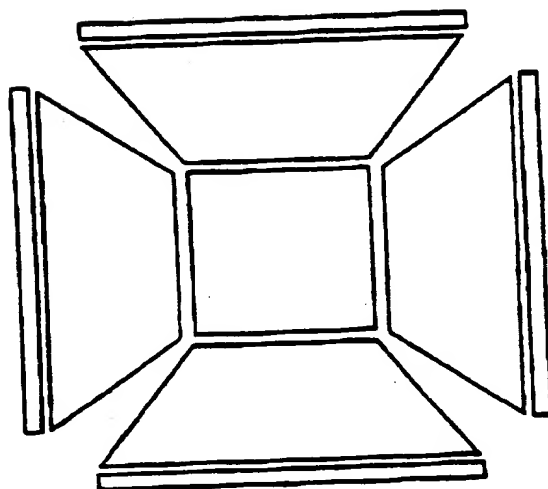


FIG. 10

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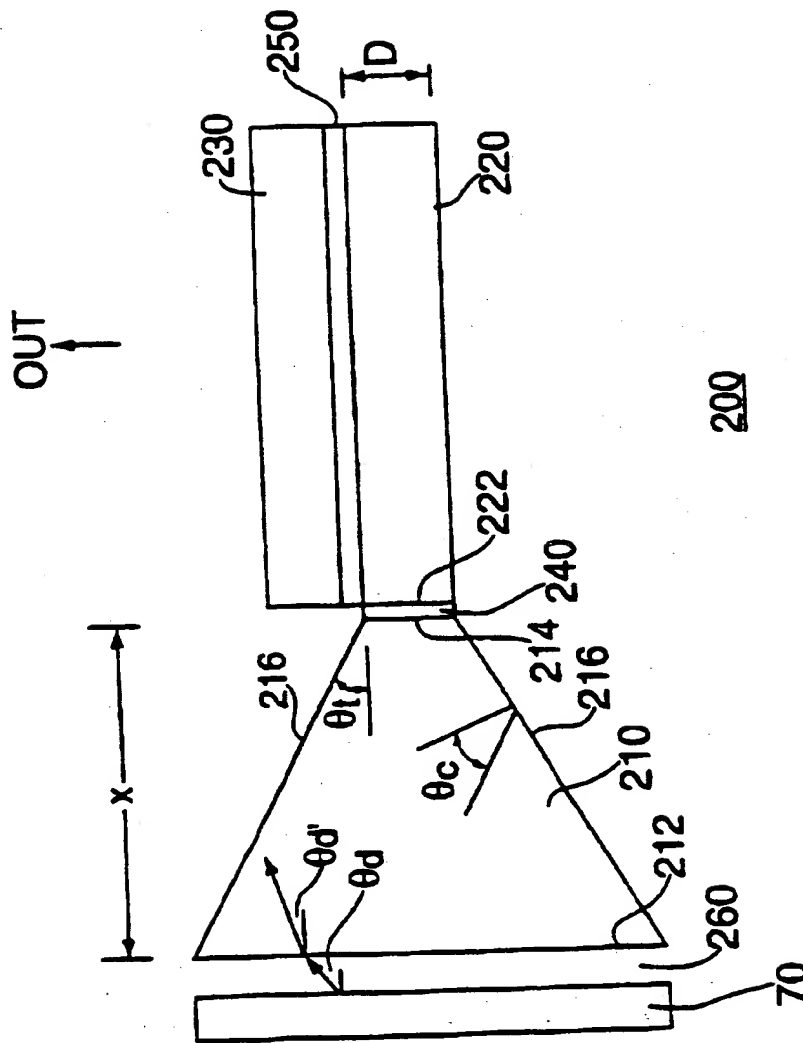


FIG. 8



# INTERNATIONAL SEARCH REPORT

Int. ional Application No  
PCT/US 97/11378

**A. CLASSIFICATION OF SUBJECT MATTER**  
IPC 6 F21V8/00 G02B6/42

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)  
IPC 6 F21V G02B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X Y A	EP 0 500 089 A (TOSOH) 26 August 1992 see page 3, line 30 - line 40; figure 2	1 2-8 9
P,X P,Y P,A	EP 0 751 340 A (LUMITEX) 2 January 1997 see the whole document	2-4 5-8 9
Y A	US RE33722 E (D.R.SCIFRES ET AL.) 22 October 1991 see the whole document	2-8 9
Y A	EP 0 192 164 A (NIPPON HOSO KYOKAI) 27 August 1986 see page 5; figure 1	6 9

☐ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

\* Special categories of cited documents :

- "A" document defining the general state of the art which is not considered to be of particular relevance
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"A" document member of the same patent family

Date of the actual completion of the international search

27 October 1997

Date of mailing of the international search report

06/11/1997

Name and mailing address of the ISA

European Patent Office, P.B. 5818 Patentlaan 2  
NL - 2280 HV Rijswijk  
Tel. (+31-70) 340-2040. Tx. 31 651 epo nl.  
Fax: (+31-70) 340-3016

Authorized officer

Malic, K

# INTERNATIONAL SEARCH REPORT

International application No

PCT/US 97/11378

## Box I Observations where certain claims were found unsearchable (Continuation of Item 1 of first sheet)

This International Search Report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:

1. ☒ Claims Nos.:  
because they relate to subject matter not required to be searched by this Authority, namely:
2. ☐ Claims Nos.:  
because they relate to parts of the International Application that do not comply with the prescribed requirements to such an extent that no meaningful International Search can be carried out, specifically:
3. ☐ Claims Nos.:  
because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a)

## Box II Observations where unity of invention is lacking (Continuation of item 2 of first sheet)

This International Searching Authority found multiple inventions in this international application, as follows:

CLAIM 1 : REFLECTOR  
CLAIM 2 : ILLUMINATOR SOURCE  
CLAIMS 3-9 : ILLUMINATOR SYSTEM

1. ☐ As all required additional search fees were timely paid by the applicant, this International Search Report covers all searchable claims.
2. ☒ As all searchable claims could be searched without effort justifying an additional fee, this Authority did not invite payment of any additional fee.
3. ☐ As only some of the required additional search fees were timely paid by the applicant, this International Search Report covers only those claims for which fees were paid, specifically claims Nos.:
4. ☐ No required additional search fees were timely paid by the applicant. Consequently, this International Search Report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:

Remark on Protest

- ☐ The additional search fees were accompanied by the applicant's protest.  
☐ No protest accompanied the payment of additional search fees.

# INTERNATIONAL SEARCH REPORT

information on patent family members

Int'l. Application No

PCT/US 97/11378

Patent document cited in search report	Publication date	Patent family members(s)	Publication date
EP 0500089 A	26-08-92	JP 4280225 A	06-10-92
		JP 4267222 A	22-09-92
		DE 69212662 D	19-09-96
		DE 69212662 T	20-02-97
		US 5262928 A	16-11-93
-----			
EP 0751340 A	02-01-97	US 5613751 A	25-03-97
		JP 9021916 A	21-01-97
		US 5618096 A	08-04-97
-----			
US RE33722 E	22-10-91	US 4763975 A	16-08-88
		US 4818062 A	04-04-89
		US 4820010 A	11-04-89
-----			
EP 0192164 A	27-08-86	JP 61188509 A	22-08-86
		CA 1273834 A	11-09-90
		US 4807954 A	28-02-89
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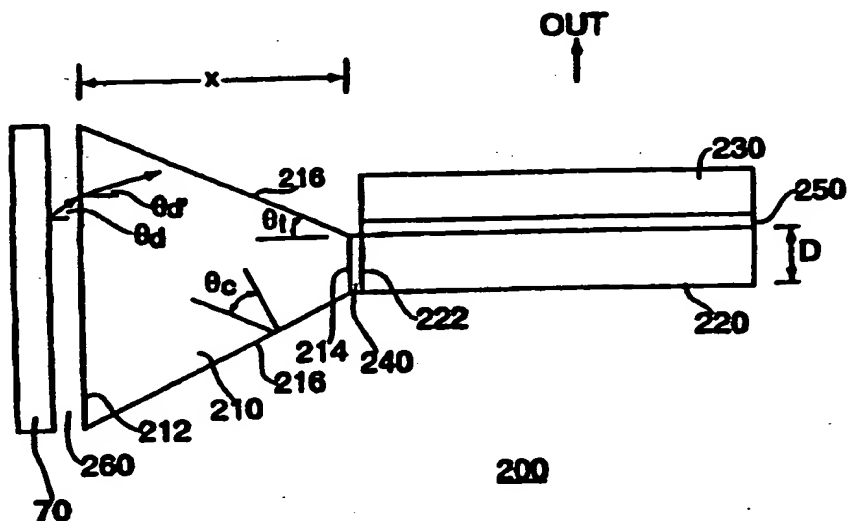
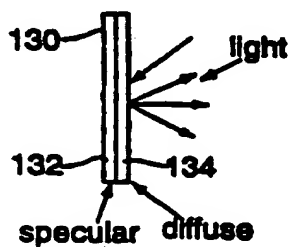
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<b>(21) International Application Number:</b> PCT/US97/11378 <b>(22) International Filing Date:</b> 1 July 1997 (01.07.97)  <b>(30) Priority Data:</b> 08/679,047 12 July 1996 (12.07.96) US  <b>(71) Applicant:</b> ALLIEDSIGNAL INC. [US/US]; 101 Columbia Road, P.O. Box 2245, Morristown, NJ 07962-2245 (US).  <b>(72) Inventors:</b> UNGER, Waltraud, Rosalie; 9 Warren Place, Glen Rock, NJ 07452 (US). ZIMMERMAN, Scott, Moore; 41 Carlisle Road, Basking Ridge, NJ 07920 (US). KUPER, Jerry, W.; 1336 Tullo Road, Martinsville, NJ 08836 (US). CHIN, Tim; 3233 Delta Road, San Jose, CA 95135 (US).  <b>(74) Agent:</b> CRISS, Roger, H.; AlliedSignal Inc., Law Dept. (C.A. McNally), 101 Columbia Road, P.O. Box 2245, Morristown, NJ 07962-2245 (US).		<b>(81) Designated States:</b> CA, JP, KR, NO, European patent (AT, BE, CH, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE).  <b>Published</b> <i>With international search report.</i>

**(54) Title:** ILLUMINATION SOURCES AND SYSTEMS

**(57) Abstract**

The reflectivity of a substrate (40) can be improved by combining a reflective diffuse layer (139) with a specular layer (132). The light output of individual light sources (70) can be improved by embedding them in a composite diffuse and specular substrate (40) resulting in a superior illumination source. A tapered coupling waveguide (210) having a large input surface (212) can be used to couple the illumination source (70) to a thin waveguide (220) having a relatively small input surface area (222).



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